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2	Improved quantification of livestock associated odorous volatile
3	organic compounds in a standard flow-through system using
4	solid-phase microextraction and gas chromatography - mass
5	spectrometry
6	
7 8 9 10 11 12 13 14 15 16 17 18	 Xiuyan Yang¹, Wenda Zhu^{1,2}, Jacek A. Koziel^{1*,3,4}, Lingshuang Cai¹, William S. Jenks⁵, Yael Laor⁶, J. (Hans) van Leeuwen^{3,1,4}, Steven J. Hoff¹, ¹ Department of Agricultural & Biosystems Engineering, Iowa State University, USA ² Interdepartmental Toxicology Program, Iowa State University, USA ³ Department of Civil, Construction & Environmental Engineering, Iowa State University, USA ⁴ Department of Food Science and Human Nutrition, Iowa State University, USA ⁵ Department of Chemistry, Iowa State University, USA ⁶ Agricultural Research Organization, Institute of Soil, Water and Environmental Sciences, Newe Ya'ar Research Center, Ramat-Yishay, Israel * Corresponding author: tel.: 515-294-4206, fax: 515-294-4250, koziel@iastate.edu

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Abstract. Aerial emissions of odorous volatile organic compounds (VOCs) are an important 20 nuisance factor from livestock production systems. Reliable air sampling and analysis methods 21 are needed to develop and test odor mitigation technologies. Quantification of VOCs 22 23 responsible for livestock odor remains an analytical challenge due to physicochemical properties of VOCs and the requirement for low detection thresholds. A new air sampling and 24 analysis method was developed for testing of odor/VOCs mitigation in simulated livestock 25 emissions system. A flow-through standard gas generating system simulating odorous VOCs 26 in livestock barn emissions was built on laboratory scale and tested to continuously generate 27 28 ten odorous VOCs commonly defining livestock odor. Standard VOCs included sulfur VOCs (S-VOCs), volatile fatty acids (VFAs), and p-cresol. Solid-phase microextraction (SPME) was 29 optimized for sampling of diluted odorous gas mixtures in the moving air followed by gas-30 chromatography mass-spectrometry (GC-MS) analysis. CAR/PDMS 85 µm fiber was shown to 31 32 have the best sensitivity for the target odorous VOCs. A practical 5-min sampling time was selected to ensure maximum extraction of VFAs and p-cresol, as well as minimum displacement 33 34 of S-VOCs. Method detection limits ranged from 0.392 to 2.64 ppbv for S-VOCs, 0.233 to 0.767 ppbv for VFAs, and 0.308 ppbv for p-cresol. The method developed was applied to quantify 35 VOCs and odorous VOC mitigation with UV light treatment. The measured concentrations 36 ranged from 20.1 to 815 ppbv for S-VOCs, 10.3 to 315 ppbv for VFAs and 4.73 to 417 ppbv for 37 p-cresol. Relative standard deviations between replicates ranged from 0.67% to 12.9%, 0.50% 38 to 11.4%, 0.83% to 5.14% for S-VOCs, VFAs and *p*-cresol, respectively. This research shows 39 that a simple manual SPME sampler could be used successfully for quantification of important 40 classes of odorous VOCs at concentrations relevant for real aerial emissions from livestock 41 operations. 42

43 Key words: VOCs, SPME, GC-MS, odor, air sampling, standard gas generation system

45 **1. Introduction**

Worldwide proliferation of intensive large-scale livestock production systems has focused 46 47 the attention on aerial emissions of odor, VOCs, NH₃, H₂S, and bioaerosols, including pathogens [1]. Livestock air emissions are a complex mixture of very dilute odorous VOCs, 48 among which several key volatile organic compounds (VOCs and semi-VOCs) were found to 49 50 be responsible for odor nuisance [2-8]. Previous studies reported three main categories of chemicals as the key odorants from swine operations, i.e., sulfur-containing VOCs (S-VOCs), 51 volatile fatty acids (VFAs), and phenolics/indoles [2,8]. Ammonia, which is characterized by 52 relatively higher odor threshold compared to most of these VOCs, and typically present at 53 higher concentrations, may or may not correlate with odor concentrations [9]. Hydrogen 54 sulfide and methanethiol were reported to represent 70 to 97% of the total sulfuric gases and 55 volatiles in manure [10]. The most dominant sulfuric gases and volatiles in cattle manure were 56 found to be hydrogen sulfide (39%), methanethiol (34%) and dimethyl sulfide (21%) [11]. 57 VFAs were reported to be major odorants for emissions associated with animal production 58 systems, more specifically, about 60% of total VFAs in manure were present as acetic acid, 59 followed by propanoic acid, butyric acid, isobutyric acid and isovaleric acid [12-14]. Bulliner et 60 al. [2] reported p-cresol as the key compound responsible for the characteristic smell of swine 61 odor. It is generally accepted that the key odorous VOCs responsible for livestock odor 62 typically present at very low levels (ppbv to pptv). 63

Quantification of odorous VOCs from livestock operations is necessary in order to develop and test various odor mitigation technologies. However, there are challenges in quantifying target odorous VOCs because of their low concentrations (typically in the ppbv range) and the extremely low odor threshold of some of these compounds (which can be in the pptv range). Moreover, the majority of odorous VOCs are present at such trace levels in a complex matrix of odor-insignificant volatiles.

Several studies reported analytical detection limits of livestock odorants (Table 1).
However, most of these were done in a static system; fewer studies aimed at quantifying
VOCs in livestock air applying flow-through systems [15]. Moreover, in most studies
summarized in Table 1, samples were stored in a polymeric bag (e.g. Tedlar) or a metal
canister [19]. Such storage devices were reported to suffer from sample contamination and
sample loss [26]. Finally, most of reported studies focused on a few target compounds, such

as S-VOCs or VFAs only.

Notably, human odor detection threshold of target VOCs selected in the present study were reported at very low concentrations, mostly below 4 ppbv except acetic (145 ppbv) and propanoic acid (35.5 ppbv), as shown in Table 2. To fulfill the experimental needs, a system capable of producing gas mixtures at such low concentrations is required and an appropriate sampling and analytical method has to be established to achieve method detection limits (MDLs) as low as possible.

83 A method for sampling and analysis of odorous VOCs in moving air simulating 84 concentrations present in exhaust air of livestock barns was optimized in this study. This method is based on solid-phase microextraction (SPME) coupled with gas chromatography-85 mass spectrometry (SPME-GC-MS). A mixture of 10 standard odorous VOCs was used to 86 simulate air emissions of livestock barns. As an illustration of the application of this analytical 87 method, the simulating gas mixture was treated in a flow-through reactor with UV light, thus 88 lowering concentrations further and challenging the method for residual concentrations as 89 well. 90

91 **2. Materials and methods**

92 **2.1. Standards and reagents**

HPLC-grade standards of S-VOCs, VFAs and *p*-cresol were purchased from SigmaAldrich (Milwaukee, WI).

95 **2.2. Standard gas generation system**

A standard gas generation system (SGG; Fig. 1) was built to generate mixtures of 96 VOCs/H₂S at concentrations typical to air emissions from livestock barns. Chemicals used 97 included H_2S and S-VOCs (methyl mercaptan, ethyl mercaptan, butyl mercaptan and dimethyl 98 99 sulfide (DMS)), VFAs (acetic, propanoic, butyric and isovaleric acid), and a phenolic compound (*p*-cresol). These target compounds are generally liquids at room temperature; 100 thus permeation tubes were used. Each chemical was generated by one permeation tube 101 (made and calibrated in-house or purchased from KIN-TEK[™] Laboratories (La Marque, TX, 102 103 USA)). All permeation tubes were made from Teflon. The permeation is a process of the gas

dissolving into the Teflon wall and evaporating from the outer surface, which is highly
 sensitive to temperature. The emission rate of each permeation tube was controlled by
 temperature [31,32].

107 Standard gas concentrations of each compound were calculated based on the emission 108 rate (E) of the permeation tube, which was determined by equation 1,

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110 Where E (ng/min) is the emission rate of each compound, Δm (ng) is the average mass loss 111 between two weighing times, and t (min) is the permeation period. The concentration of each 112 compound was estimated using equation 2,

 $E = \frac{\Delta m}{t} \quad (1)$

113 $C_{gas} = \frac{E}{Q} \quad (2)$

Where
$$C_{gas}$$
 is the concentration of compound of interest (ng/mL), Q is air flow rate in the

115 system (mL/min).

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To be comparable with most literature data, gas concentration were converted to volume concentration by equation 3,

119

$$C_{ppm} = C_{gas} \times \frac{R \times T}{MW \times P}$$
(3)

Where C_{ppm} is gas concentration in parts per million (ppmv), *R* is ideal gas law constant, *R*= 8.314 (m³ Pa K⁻¹ mol⁻¹), *P* and *T* are atmospheric pressure (*P*=101.32 kPa under atmospheric conditions) and temperature (K), respectively, and *MW* is the molecular weight of each compound (g/mol). Since experimental conditions were normalized to *T*=298 (K) (25 °C), and *P*=101.32 (kPa). Equation 3 can be simplified to equation 4

125
$$C_{ppm} = C_{gas} \times \frac{8.314 \times 298}{MW \times 101.32} = 24.4 \times \frac{C_{gas}}{MW} \quad (4)$$

126 Where C_{gas} was gas concentration in ng/mL calculated from Eq. 2.

Under constant temperature, different gas concentrations could be achieved by changing
 the airflow, according to Equation (2). Successful generation of constant VOCs (VFAs and
 phenolics) emissions at trace levels deploying the permeation tube technology was reported
 previously [35].

131 Differing concentrations were achieved by changing the air flow rate, i.e., the maximum concentration corresponding to 300 mL/min of air flow and the minimum concentration 132 corresponding to 5000 mL/min (Table 2). The carrier gas was 99.995% pure air (pure oxygen 133 or pure nitrogen are optional carrier gases based on experimental needs). These 134 concentrations were controlled precisely using mass flow controllers (Aalborg, Orangeburg, 135 NY). The stability of generating consistent standard gas was checked by running gas samples 136 137 daily (n=3) and continuously for 44 days. Stability was validated, as the deviation between days within the experimental period for all target analytes was small (<10%). A summary of 138 gas concentrations and physicochemical properties for all target compounds is presented in 139 Table 2. 140

This system successfully simulated the continuous emissions of VOCs from livestock 141 operations at their typical ranges of concentrations [16]. Gas concentrations generated fell 142 143 into or were very close to the typical range of odorant concentrations emitted from livestock swine facilities in North Carolina (0.075 mg/m³ (30.5 ppbv) for acetic acid, 0.04 mg/m³ (13.2 144 ppbv) for propanoic acid, 0.22 mg/m³ (60.9 ppbv) for butyric acid and 0.015 mg/m³ (4.15 145 ppbv) for isobutyric acid; 0.041 mg/m³ (9.25 ppbv) for *p*-cresol) as reported by Schiffman et. 146 al. [22]. Emissions of p-cresol from dairy farms was reported to be in the range of 0.6~100 147 µg m⁻³ [23] which can be converted to 0.14~23.8 ppbv, assuming atmospheric conditions. Not 148 much information about measured concentrations of sulfur VOCs was found in the literature, 149 probably because field concentrations were below their detection threshold [22], while a range 150 of 0.064-0.927 ppbv was reported for dimethyl sulfide emitted from a slurry wastewater 151 152 lagoon [18].

2.3. Headspace solid phase microextraction (HS-SPME)

All HS-SPME extractions were performed with a SPME fiber coupled with a manual holder 154 from Supelco (Bellefonte, PA, USA). Before use, each fiber was conditioned in a heated GC 155 splitless injection port at 260 °C under helium flow. After conditioning, SPME fiber was quickly 156 moved to the sampling ports to perform extractions as required. Once air samples were 157 collected, the SPME fiber was removed and immediately transferred to the injection port of 158 159 the GC for analysis. The desorption time of SPME fiber was set to 10 min at 260 °C. All 160 SPME extractions were completed at constant temperature (see section 2.5). The sampling time was optimized (described in section 2.6). 161

162 **2.4. SPME fiber selection**

Four SPME fiber coatings, Carboxen/polydimethylsiloxane (CAR/PDMS) 85 μm,
 PDMS/divinylbenzene (DVB0 65 μm, polyacrylate (PA) 85 μm and PDMS 100 μm were
 examined in this work to select a fiber coating with the best extraction efficiency on target
 VOCs. All samples were taken in triplicate at 25 °C from SGG by headspace SPME fiber.
 Carrier air was dry. Gas flow rate was set constant at 300 mL/min.

Fiber selection was conducted for standard odorous gases in the SGG to select the SPME coating with best trapping capacity of target analytes. This part was done within 48 h with constant airflows and temperature (constant gas concentrations) in the SGG. Three replicated samples were taken continuously for each fiber coating. The sampling time was 5 min (Section 2.6).

173 **2.5. Sampling time optimization**

Out of the four fiber coatings, CAR/PDMS 85 µm was chosen for the optimization of sampling time. Sampling times of 1, 3, 5, and 10 min were examined for standard odorous gases in the SGG with triplicates. Partitioning coefficient, molecular size and boiling point are considered important factors influencing equilibration time [37]. Since the CAR/PDMS phase is adsorptive [38], sampling time was optimized by selecting the longest extraction time before fiber sorptive capacity limits the rate of analyte extraction.

180 **2.6. Method application to photoreactor**

The developed method was challenged by applying it to odor mitigation technology by means 181 of a photoreactor. The effluent from the SGG (Section 2.2) was fed to a flow through chamber 182 which was used as the photoreactor using variable numbers of low-pressure Hg lamps 183 (principle output at 254 nm, with other characteristic bands at 185, 312 and 365 nm). The 184 reactor contained TiO₂ as photocatalyst, and included a temperature control sensor, and an 185 on/off switch. When the UV source was on, photodegradation of gases was induced. When the 186 UV light was off, the photoreactor functioned simply as a flow through cell. More details about 187 188 the UV photoreactor are described in Yang et al. [36]. Sampling ports were located before and after the photoreactor to allow sampling of untreated and treated flow of standard gas mixtures 189

(shown in Fig. 1). All samples were taken in triplicates, while six replicates were used for methodvalidation.

192 **2.7. Analytical methods**

193 2.7.1 Chemical and odor analysis: GC-MS

A conventional GC–MS (Agilent 6890N GC/5973 MS from Agilent, Wilmington, DE, USA) was utilized in this study. A non-polar pre-column and a polar column were installed in series in the system. All samples were analyzed by the system under the following configuration conditions: injector 260 °C; FID, 280 °C, column oven, 40 °C initial, 3 min hold, 7 °C /min, 220 °C final, 10 min hold. Carrier gas was helium. Mass (molecular weight)-to-charge ratio (*m*/*z*) range was set between 33 and 280. Spectra were collected at 6 s and electron multiplier voltage was set to 1000 V. The MS detector was auto-tuned weekly.

Target compounds in this work were sampled and run on to GC-MS for analysis. Retention time (RT) was determined for each compound. To improve accuracy, single ion mode (SIM) was used when identification of compounds was not required. Identification was needed for the treated gases, and compounds were positively identified by two criteria: (1) the retention time on the GC capillary column, and (2) the match between the mass spectra of analyte and standard spectra in MS library from Bench-Top/PBM (from Palisade Mass Spectrometry, Ithaca, NY, USA). VOC abundance was measured as area counts under the MS peak.

208 2.7.2 Linearity, repeatability and method detection limit (MDL)

The new method repeatability was estimated at different standard gas concentrations by 209 varying air flow rate in SGG, including five levels for sulfur VOCs, nine for VFAs, and eleven 210 for p-cresol. All tests were conducted in triplicate, except at air flow of 500 mL/min (conducted 211 in 7 replicates), when MDL was estimated. The quantification of target VOCs was completed 212 by establishing calibration curves deploying the standard gas concentrations. The 213 repeatability and the calibration curves were studied under the optimized SPME conditions. 214 All extractions were done under experimental conditions of 25 °C, dry air, 5 min sampling time 215 216 and using CAR/PDMS 85 µm fiber. Precisely controlled air flow varied from 300 to 2300 mL/min. Data were analyzed and compared using means and relative standard deviations 217

(RSDs).. MDL was calculated based on the US Environmental Protection Agency (EPA)
 methodology [40]. The MDLs were defined as the minimum concentration of a substance that

can be measured and reported with 95% confidence when the analyte concentration is

greater than zero and is determined from analysis of a sample in a given matrix containing the

analyte. The MDLs for target compounds were estimated using equation 5,

223
$$MDL = s \times t_{(n-1, 1-\alpha)}$$
 (5)

where n = number of replicates. Replicates with standard analytes at concentration 1–5 times greater than the estimated MDL were generated from the SGG system; s = standard deviation of measured concentrations of n spike determinations, t = Student's *t*-value at n-1 degree of freedom and $1-\alpha$ (equals to 95%) confidence level. In this work, n=7 replicates (t-value=2.57) for *p*-cresol and n= 6 replicates (t-value=2.45) for all other target VOCs.

229 2.7.3 Statistical analysis

Detection limit and repeatability data were analyzed using the statistical package JMP v. 10.0.0 (SAS Institute, Inc., Cary, NC). Data were subject to a one-way analysis of variance (ANOVA). Correlation coefficients of the calibration curves and *p*-values between sample extractions with different fibers were calculated with Microsoft Excel.

3. Results and discussion

235 3.1 SPME fiber selection

Comparison of extraction efficiency of target VOCs for CAR/ PDMS 85 µm, PDMS/DVB 65 236 μm, PA 85 μm and PDMS 100 μm SPME coatings is illustrated as MS detector response for 237 each compound in Fig. 2 (Table S1, Supplemental Material). All the four SPME fiber coatings 238 performed sufficiently effective extraction on all selected VOCs except of sulfur compounds. 239 240 More effective extraction was observed using CAR/PDMS 85 µm and PA 85 µm fiber coatings than the other two for all target compounds, except for p-cresol, for which PDMS/DVB 65 µm 241 242 was superior. Comparison between the mixed phase coating CAR/PDMS 85 µm and the 243 single phase coating PA 85 µm indicated that CAR/PDMS 85 µm would be a better choice due to: 1) more effective extraction of all target compounds except DMS; 2) consistency with 244

one of the selection guidelines [38] that mixed phase coatings are considered to fit volatile 245 compounds sampling better than single phase coatings. One of the odor indicators for swine 246 247 manure is p-cresol [2,6.39], whose extraction efficiency is considered very critical. However, the difference in extraction efficiency between CAR/PDMS 85 µm and PDMS/DVB 65 µm on 248 *p*-cresol was not statistically significant (p=0.166), while very significant difference (p=0.009) 249 was observed for these two coatings in extracting S-VOCs and VFAs. CAR/PDMS 85 µm 250 251 captured more VFAs than PDMS/DVB 65 µm under the same conditions. Hence, CAR/PDMS 85 µm coating can be more effective in extracting a wider range of compounds. PDMS/DVB 252 65 µm also had a poor performance in trapping S-VOCs. Sulfur VOCs at trace levels, even 253 below the detection limit, contribute significantly to the total odor [25], and is another critical 254 group of VOCs associated with livestock odors. According to Pawliszyn [38], one important 255 principle in developing methodology is that the primary consideration should be given to the 256 257 group of analytes that is most difficult to extract and should be based on overall extraction efficiency. Hence CAR/PDMS 85 µm coating was selected to do all the following extractions in 258 this study. 259

The fiber selection was further justified by comparing the MS detector response RSD (%) ranges to standard concentrations of target VOCs sampled with four SPME fibers (Table 3). The RSD (%) ranged from 4.9% to 19.3% for the four fibers used. The relatively small RSD associated with the use of CAR/PDMS 85 µm coating showed good reproducibility and more stable performance for all extractions. The RSD range (from 3.3% to 7.8%) was more favorable compared with that for all the other fiber coatings.

3.2. Selection of sampling time

The sampling time optimization was conducted for CAR/PDMS 85 µm fiber. Experiment 267 was performed in triplicates at a 5-point time series basis ranging from 1 min to 1 h. The 268 mean FID response was plotted against extraction time. Detected peak area (PA) counts 269 increased with sampling time in a linear trend for most compounds except for methyl 270 mercaptan after 10 min extraction, when it started to deviate from linearity. However, when up 271 to 10 min was selected, all target odorants showed a high positive linearity between extracted 272 mass and extraction time (Fig. 3). The correlation coefficient R² values for VFAs and *p*-cresol 273 nearly equal to 1 (Table 4). According to Pawliszyn [38], the practical sampling time should be 274

the longest extraction time with the maximum amount extracted before the extraction reaches 275 equilibrium. However, CAR/PDMS extracts analytes by adsorption, which means a 276 277 competitive adsorption of VOCs to the surface of the fiber coating. With lower affinity to CAR/PDMS, S-VOCs tend to be easily replaced. None of previous research analyzed S-278 279 VOCs, VFAs and *p*-cresol simultaneously, thus not dealing with a range of molecular weight compounds and functionalities with differing affinities to the fiber. Efficient extraction of S-280 281 VOCs in a complex gas mixture (of target VOCs) needs to be assured. Non-linear extraction conditions for S-VOCs are less useful for quantification, are difficult to control and not 282 recommended for quantitative analysis. A shorter extraction time in a linear extraction range 283 was considered. Good reproducibility was observed for target VOCs (RSD less than or close 284 to 5%) for up to 5 min extraction (Table 4), and, at the same time, the risk of non-linear 285 extractions and fiber coating saturation was minimized. This shorter extraction time (5 min) is 286 287 also more practical in the sense of time saving for sampling. Hence 5 min extraction was chosen for most of the analyses in this work. 288

289 Further comparison was illustrated by plotting the FID detector response normalized by gas concentrations over sampling time for each compound (Fig. 3). The slope m represents 290 291 FID response normalized by gas concentrations as a function of air sampling times with SPME. The relationship between normalized peak area (PA) counts and sampling time 292 293 followed four salient trends: 1) comparison among all three groups (S-VOCs, VFAs and pcresol) showed that the slope m* increased with molecular weight except for ethyl 294 mercaptan/DMS and the isomer isovaleric acid; 2) comparison within each group showed a 295 steadily, if not linearly, increasing trend between the slope m* and molecular weight except for 296 isovaleric acid as shown in Fig. S1, and the correlation coefficients were 0.96 and 1.00 for S-297 VOCs and VFAs, respectively; 3) more rapid increase was observed for VFAs than S-VOCs 298 compounds; 4) *p*-cresol was the compound with much higher m^{*} than the other analytes. 299 RSD (%) and linearity of FID response to standard concentrations of target VOCs sampled 300 with SPME fiber at different air sampling times are summarized in Table 4. 301

302 **3.3**. Method evaluation and validation

The optimized procedure was evaluated and validated based on its linearity, detection limit, repeatability and recovery. The linearity of the method was evaluated by preparing

305 calibration standards generated by SGG. The calibration curves were linear over the concentration ranges of target analytes as shown in Fig. 4. The linear regression equation 306 coefficients, range of the gas concentrations, R², method detection limits (MDLs) and ranges 307 308 of RSDs (%) are summarized in Table 5. MDLs were estimated based on 6 replicates (7 for pcresol). Up to 1 ppbv MDL was achieved for most of the compounds except methylmercaptan 309 and ethylmercaptan. The lowest MDL was 0.233 ppbv for butyric acid, while the MDL of p-310 cresol was 0.308 ppby, which covers the range of typical aerial concentration of p-cresol in 311 livestock emissions [16, 41]. 312

313 3.4. Method application for analysis of odorous VOCs in moving air irradiated with UV

An example of a total ion chromatogram of UV treated gas sample from SGG is shown in Fig. 5. VOC concentrations were calculated using the calibration curves (Table 6). The concentrations of all VOCs were in the range of the maximum measured concentrations calculated by calibration curves and the MDLs. In this demonstration of odor mitigation by means of UV, measured concentrations of key odorants were reduced by approximately 40 to 70%.

320 **4. Conclusions**

Headspace-SPME coupled with GC–MS is a useful and effective analytical tool for characterization and quantification of complex odorant mixtures associated with livestock operations. The low detection limits (ranging from 0.23 to 2.64 ppbv) obtained with the optimized method were approximately one order of magnitude below published detection thresholds for target odorous gases.

Extraction of sulfur VOCs, VFAs and *p*-cresol with SPME were optimized simultaneously for the first time. The CAR/PDMS 85 µm extraction efficiency was positively correlated with molecular weight of target compounds of the same chemical functionality. Methyl mercaptan, ethyl mercaptan, and dimethyl mercaptan at low molecular weights have the lowest affinity to the SPME fiber. Extraction efficiency of these compounds with low affinity to SPME fiber was optimized by shortening extraction time.

332 Acknowledgements

The authors would like to thank National Pork Board and United States-Israel Binational Agricultural Research and Development (Project No.US-3999-07) for funding this research.

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443 **Figure Captions**

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Fig.1. A Scheme of the standard gas mixture generation system (SGG) coupled with a benchscale UV photoreactor.

Fig.2. Comparison of extraction efficiency of target VOCs for different SPME fibers coatings: CAR/PDMS 85 μ m, PDMS/DVB 65 μ m, PDMS 100 μ m and Polyacrylate 85 μ m. MS detector response was normalized by gas concentrations. SPME conditions: T = 25 °C, sampling time = 5 min, flow rate = 300 mL/min, dry air. Abbreviations: methyl mercaptan = MeSH, ethyl mercaptan = EtSH, dimethyl sulfide = DMS, n-butyl mercaptan = BM, acetic acid = AcOH, propanoic acid = PPA, butyric acid = BTA, isovaleric acid = IVA.

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- Fig.3. Optimization of SPME sampling time of target VOCs from standard gas mixture:
 normalized by gas concentrations. Experimental conditions: CAR/PDMS 85 μm SPME fiber,
 300 mL/min standard gas flow, T=25 °C, dry air. Five min sampling was selected for all followup experiments.
- Fig.4. Calibration curves for target VOCs. Experimental conditions: gas sampling with
 CAR/PDMS 85 μm; 5 min sampling time; T=25 °C; dry air.

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Fig. 5. Comparison of total ion chromatograph of treated gas sample with control sample from SGG. Experimental conditions: gas sampling with CAR/PDMS 85 μ m; 5 min sampling time; T=25 °C; dry air; flow rate = 300 ml/min; UV treatment at 254 nm (principle) and 185 nm, with light intensity = 1.5 mW/cm² @254 nm with TiO₂ present. Note: MM=methyl mercaptan, EM=ethyl mercaptan, DMS=dimethyl sulfide, BM=butyl mercaptan, AA=acetic acid, PA= propanoic acid, BA=butyric acid, IV=isovaleric acid.